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For: Apparatus and Method of Making a Droplet Target

**English Translation of Applicants' Original German Specification
Including Their Preliminary Amendment of 13 June 2005
with Brackets and Underlining Deleted**

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5 Apparatus and Method of Making a Droplet Target

BACKGROUND OF THE INVENTION.

1. Field of the invention.

10 The invention relates to an apparatus for making a droplet target provided with at least one receptacle for receiving the target liquid in which a high pressure is realized by means of gaseous nitrogen, a magnetic valve connected to the receptacle and switchable in the ms range, and a nozzle, as well as to a method.

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2. The Prior Art.

 Hereafter, devices known in the prior art will be described by which liquid droplets are being generated wherein the interaction of laser beams
20 aimed at these droplets generates X-rays or extreme ultra-violet light. Such rays are used, for instance, in microscopy and lithography.

 U.S. patent No. 6,324,256 describing an arrangement of a laser plasma source for generating EUV light, also refers to a device for making
25 droplet targets. The droplets made are of a diameter larger than the diameter of droplets generated by a gas fed through a nozzle where it condenses to form a cloud of clusters of extremely small particles. As described, a liquid is formed from the gas by means of a heat exchanger which reduced the temperature of the gas. The liquid is fed to a nozzle the opening of which
30 increases in the direction of the exit opening. The droplets are formed in this section and then exit from the exit opening of the nozzle to interact with a laser beam for generating EUV light. However, it is not possible in this

arrangement in a defined manner to set the size of the droplets. In this arrangement the gaseous initial material is converted to a liquid one. Moreover, the droplets interact with the laser very close to the nozzle which in consequence of the heat and erosion is destroyed.

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In Opt. Common. 103, 105 (1993), L. Ramble and H. M. Hertz report on an X-ray source in which droplets of ethanol are used as the target. To generate these droplets, ethanol was pressed at 30 to 50 at into a vacuum chamber through a capillary of about 10 μm diameter tapering in the direction
10 of the nozzle. In order to generate a liquid volume - in this case of a diameter of 15 μm - pressure surges were piezo-electrically produced at a frequency of about 1 MHz. The relatively large droplets were used for examining the interaction with laser radiation in an intensity range of 10^{12} to 10^{14} W/cm² as described by O. Hemberg, B. A. M. Henson, M. Berlund and H. M. Hertz in J.
15 Appl. Phys. 88, 5421 (2000). Since in this case each individual droplet is interacting and the laser focus is but slightly larger than the diameter of the droplets of ethanol, the drift problem of the droplet source is of major importance, the project is especially directed to solving an exact droplet-laser synchronization.

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Super dense droplet spray of a density of up to 10^{19} atoms/cm³ and a droplet diameter of about 1 μm was produced by a droplet source described by L. C. Mountford, R. A. Smith and M. R. H. R. Hutchinson in Rev. Sci. Instrum. 69, 3780 (1998) and is the basis of the instant invention. The basis
25 of this droplet source is a magnetic valve which forms the pulse of liquid and, therefore, the volume of the liquid. A receptacle was filled with a liquid and kept under high pressure by means of methanol. The valve is opened in synchronism with the laser pulse and for 2,500 μs to allow droplets to emerge from the nozzle. It was possible to produce droplets of lesser diameter of
30 about .6 μm by subsequent electrostatic cleaving of the droplets. This, however, requires a technically complex arrangement. However, the jog consisting of such droplets is of lower density, viz. about 10^{16} atoms/cm³.

For effectively generating X-rays or EUV light it is necessary, however, to make available droplet targets of dimensions of the size of possible laser wavelengths (T. D. Donnelly, M. Rust, I. Weiner, M. Allen, R. A. Smith, C. A. Steinke, S. Wilks, J. Zweiback, T. E. Cowan, and T. Ditmire, J. Phys. B: At. Mol. Opt. Phys. 34, L313 (2001)) and, therefore, of a smaller diameter compared to the prior art, and which form a spray of an atomic density of $> 10^{18}$ atoms/cm³.

OBJECT OF THE INVENTION.

It is thus an object of the invention to provide a way by which such droplet targets can be produced. The high density is also to be realized at a greater distance from the nozzle, i.e., the droplet target, compared to the prior art, is of a superior collimation in order to extend the useful life of the nozzle.

SUMMARY OF THE INVENTION.

The object is accomplished with an apparatus of the type referred to *supra* in which the nozzle, in accordance with the invention, is constituted by an supersonic nozzle, the valve is connected to the supersonic nozzle by an expansion channel, heating means are formed around the expansion channel such that the temperature may be set at a level at which a super saturated vapor is generated in the expansion channel, and an insulation is provided between the electromagnetic valve and the heating means.

The invention makes possible the generation of super dense sub- μ liquid targets required for examining the interaction between laser radiation and plasmas. In contrast to the mentioned prior art generating droplets in the saturated gas phase, the droplets in accordance with the invention are generated from super saturated vapor which condenses into a cloud of spray. The target generated by the apparatus of the invention consists of droplets of an mean diameter of about 150 nm and is of an mean atomic density of $>$

10¹⁸ atoms/cm³. Such a target makes it possible the examination of conditions hitherto not researched which exist between clusters (from several atoms to 10¹⁶ atoms/cluster of a local density approximating that of a solid) and solids. Moreover, relative to the advantages of a cluster target, the
5 spatial extent of the droplets influences an increased volume charge limitation of hot electrons which, in turn, results in an improved coupling of the laser energy with the ions of the droplets. Thus, a much hotter plasma can be generated and the effect in the X-ray conversion can be improved. The droplet target produced with the device of the invention can be generated
10 continuously and is of chronologically unlimited operation.

Embodiments of the apparatus in accordance with the invention relate to the structure of their individual components. The pulsed electromagnetic valve operates at a pulse length of 2 ms; the length of the expansion channel
15 is from several mm to several cm and its diameter is from several 100 μm into the mm range; the supersonic nozzle has a conical opening angle 2Θ from several degrees to several 10°, an input opening of several 100 nm diameter and a conical section of a length of several mm. After pressing the target liquid upon opening of the valve into the expansion channel where as a result
20 of the heating a supersaturated water vapor is present, it will expand during passage through the ultrasonic nozzle, cool, and form liquid droplets of the desired size and density, the parameters being determined by the dimensions of the expansion channel, its temperature and the prevailing pressure in it.

25 The method in accordance with the invention includes the following method steps: Filling of a target liquid into a container, in which a high pressure is realized by means of a non-reactive gas, brief opening of the receptacle by a pulsed electromagnetic valve, pulsed introduction of the target liquid into an expansion channel, heating of the expansion channel
30 such that a supersaturated liquid vapor is generated, cooling of the vapor during passage to a supersonic valve connected to the expansion channel, discharge of the droplets from the output opening of the nozzle into a

vacuum.

In some embodiments of the invention a pulsed electromagnet valve is used operating in the ms range and, more particularly, at a pulse duration of 2
5 ms. At each switching of the valve the target liquid is pressed into the expansion channel and the corresponding vapor is pressed into the supersonic nozzle. An expansion channel of several mm to several cm in length and a diameter of several 100 μm to the mm range and a supersonic nozzle of with a conical opening angle 2Θ of several degrees to several 10° ,
10 an input opening of several 100 μm diameter and a conically shaped section several mm in length are used. During its passage to the discharge opening of the nozzle the supersaturated gas is cooled in the nozzle. This leads to the formation of liquid droplets. It is further to be mentioned that in addition to the mentioned parameters of the expansion channel the diameter of the nozzle
15 also determines the diameter of the liquid droplets emerging from the nozzle opening into the vacuum.

Compared to the prior art which constitutes the basis of the invention, the valve in accordance with the invention regulates the direct feeding into an
20 additionally provided expansion channel in which the target liquid is heated. The thus present supersaturated gas is fed to the discharge opening of the nozzle and cooled which leads to the formation of droplets in the nozzle. By contrast, in the known arrangement, the valve switches the nozzle directly into its closed and open states which substantially lessens the effect on the
25 formation and extent of the droplets and their collimation.

DESCRIPTION OF THE SEVERAL DRAWINGS.

The novel features which are considered to be characteristic of the
30 invention are set forth with particularity in the appended claims. The invention itself, however, in respect of its structure, construction and lay-out as well as manufacturing techniques, together with other objects and advantages

thereof, will be best understood from the following description of preferred embodiments when read in connection with the appended drawings, in which:

Fig. 1 schematically depict the structure of an apparatus in accordance with
5 the invention;

Fig. 2 is a curve of the switching pulse of the valve and the associated
intensity of the liquid spray generated as a function of time;

Fig. 3 is a curve of the width of expansion of the liquid spray in air and in
vacuum as a function of the distance from the discharge opening of the
10 nozzle;

Fig. 4 is a curve of the density of the liquid spray as a function of the distance
from the discharge opening of the nozzle; and

Fig. 5 is a curve of the relative intensity of scattered light measured by CCD.

15 DESCRIPTION OF THE PREFERRED EMBODIMENT.

The apparatus in accordance with the invention for generating a droplet target is provided with a pulsed electromagnetic valve 1. The valve closes a receptacle (not shown), in which target liquid is maintained at a
20 pressure of 35 bar by gaseous nitrogen. The target liquid may be water, but in principle it may be any other liquid as well. The valve 1 opens and closes at a pulse duration of 2 ms and, in its open phase, discharges water droplets into an expansion channel 2 of 1 mm diameter and 15 mm length. By means of a heater 3 a temperature of 150 °C is generated in the expansion channel
25 2. The expansion channel 2 is separated from the valve 1 by an insulator 5. The supersaturated water vapor now present at the end of the expansion channel 2 is now fed through a supersonic nozzle 4. The nozzle 4 has an opening angle of $2\Theta = 7^\circ$, an input opening of 500 μm diameter and a conical section of 8 mm length and generates sub- μ liquid droplets into the vacuum.
30 A droplet target which can be continuously generated and which makes possible a chronologically unlimited operation is formed at the discharge opening of the supersonic nozzle 4.

Fig. 2 displays a curve of the switching pulse of the valve and the associated intensity of the generated liquid spray as a function of time at a distance of 1 mm from the discharge opening of the nozzle. In this measurement during which the radiation generated by a cw He-Ne-laser was directed to and scattered by the droplet target, and the intensity of the scattered radiation at a spacing of 1 mm from the nozzle opening was determined, the pulse duration of the valve was 2 ms. It can be seen that the major portion of the spray pulse occurs about 1 ms after opening of the valve.

Fig. 3 shows a curve depicting the spread of the liquid spray as a function of distance from the discharge opening of the nozzle in air and in vacuum. Compared to results known from the prior art, it can be seen that the collimation resulting in accordance with the invention is improved by about 30%.

The spread geometry of the generated cloud of droplet spray may be defined as $R = (.32 \pm .32) \times h + r$, R being the radius of the spray/fog cloud, h being the distance from the supersonic nozzle and r being the radius of the discharge opening of the supersonic nozzle. A zero distance corresponds to the discharge opening of the supersonic nozzle.

Fig. 4 discloses a curve which depicts the dependency of the density of the droplets within the spray as well as the dependency of the mean atomic density in the spray upon the distance from the discharge opening of the nozzle. The measured droplet density varies as regards droplets of a .15 μm diameter from $(1.6 \pm .5) \cdot 10^{11}$ droplets per cubic centimeter (or a mean molecular density of $8 \cdot 10^{16} \text{ cm}^{-3}$) at a distance of 20 mm from the discharge opening. At this droplet size this constitutes a droplet density higher by up to three orders of magnitude than in currently described spray droplet source. This is important for the conversion of irradiated laser energy.

Fig. 5 depicts the measurement data of the scattered light intensity as

a function of the viewing angle. The solid line represents the theoretical distribution of the scattered light intensity of particles of a diameter of .15 μm . The correspondence with the measurement data indicates a closer distribution of the droplet sizes than in the prior art so that - unlike in the prior art - there is no need for a droplet size filter and that in this manner the effective droplet density is advantageously increased.

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What is claimed is: